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# Simultaneous Decolorization of Tartrazine and Production of H<sub>2</sub> in a Combined Electrocoagulation and Photocatalytic Processes using CuO-TiO<sub>2</sub> Nanotube Arrays: Literature Review and Experiment

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## ABSTRACT

We reported the simultaneous decolorization of tartrazine and H<sub>2</sub> production via electrocoagulation and photocatalysis using CuO-doped TiO<sub>2</sub> nanotube arrays (TNTA) composites. Tartrazine was removed by the combination of adsorption, electrocoagulation, and photocatalytic degradation, while H<sub>2</sub> was produced through water reduction at the cathode and water splitting process on the photocatalyst surface. The photoreactor contains CuO-TNTA as a photocatalyst and is equipped with an 80-W UV lamp. Deposition of CuO on TNTA was conducted using a successive ionic layer adsorption and reaction (SILAR) method. The nanotubular of the TNTA as well as the distribution of CuO were evaluated employing FESEM and HRTEM. XRD patterns confirmed weak diffraction of CuO and TNTA revealing an anatase crystallite phase. The band gap of the CuO-TNTA was also found to be redshifted from that of pure TNTA. The simultaneous processes with the combined systems (20 V, pH = 11) managed to remove 80% of tartrazine while producing a high H<sub>2</sub> yield (1.84 mmol), significantly higher than those obtained by each process.

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#### 1. INTRODUCTION

The textile and food industries use organic dyes in their manufacturing processes which have become major environmental and health problems due to the toxicity and carcinogenic nature of the dyes (Soufia et al., 2022). Dyes are organic pollutants that have triggered many concerns because they are difficult to remove from wastewater streams (Popli & Patel, 2015). For example, is tartrazine (C<sub>16</sub>H<sub>9</sub>N<sub>4</sub>Na<sub>3</sub>O<sub>9</sub>S<sub>2</sub>) or acid yellow 23, which is a harmful azo and anionic dye commonly used for food coloring, pharmaceuticals, plastics, fibers, and paper (Vaiano et al., 2016; Okoniewska, 2021). Long-term consumption of foods containing tartrazine will potentially cause cancer, asthma, diarrhea, and hyperactivity in children that may interrupt their cognitive development (Vaiano et al., 2016; Amin & Al-Shehri, 2018). Therefore, it is imperative to find ways through which tartrazine is eliminated to an acceptable level using affordable and appropriate technology. According to Regulation of the National Agency of Drug and Food Control (BPOM) No. 37, the concentration of tartrazine must be reduced to at least 7.5 mg/L before it is safely disposed of to the environment.

Achieving the mentioned goals is by no means a trivial task, as many techniques have been studied without definitive success. Biological treatments are ineffective in removing tartrazine since the dye is nonbiodegradable (Vaiano et al., 2016). The adsorption method is often deemed inappropriate because it only captures the pollutant without converting it to harmless entities (Gupta et al., 2011). Physical and chemical treatments have also been implemented, however, problems related to sludge formation during the process create new problems because it harms the environment (Gupta et al., 2011). Moreover, dye is a substance that is difficult be oxidized due to its large molecule size and complex structure. Several other techniques to

eliminate tartrazine have also been conducted such as ion exchange, membrane separation, adsorption, catalytic degradation (Russo et al., 2021; Soufia et al., 2022), and various advanced oxidation processes/AOPs, such as UV/H<sub>2</sub>O<sub>2</sub> (Scott *et al.*, 2017). Many dye wastes can be degraded by the AOPs which use strong oxidants like ozone  $(O_3)$ , peroxide hydrogen  $(H_2O_2),$ irradiation (UV/solar light), catalysts (metal oxides), or the combination thereof (Pourgholi et al., 2018; Javaid & Qazi, 2019). Catalytic oxidation of dyes requires active hydroxyl radicals that can be generated from, for instance, a Fenton process using iron or noniron metal catalysts (Javaid & Qazi, 2019). However, the challenges in realizing an effective method still stand, and further developments are inevitable to design more cost-effective alternatives.

One of the most promising alternatives is electrocoagulation, which is simple, rapid, cost-effective, and easy to operate. Electrocoagulation is capable of effectively eliminating tartrazine from wastewater by coagulating the colloidal waste (Pelawi et al., 2019), while also producing  $H_2$  gas which is a highly desired clean fuel (Ratnawati et al., 2014). However, the electrocoagulation system still has some drawbacks in terms of limited adsorption capacity, although it is still widely used for the degradation of dyes (Anantha Singh & Ramesh et al., 2013; Amri et al., 2020). Therefore, the formed coagulant still needs to be processed to avoid environmental problems. It is also important to note that it requires periodical replacements of the anodes because they are dissolved in the solution due to oxidation (Hashim et al., 2020).

One promising strategy to solve the mentioned problem is by combining the process with photocatalysis which can degrade pollutants chemically and, at the same time, produce  $H_2$ . Indeed, the utilization of solar energy in photocatalytic reactions has been studied extensively in the last decade, especially with a focus on its

ability to degrade organic wastes such as tartrazine (Gupta et al., 2011; Vaiano et al., 2016; Aoudjit et al., 2020), and simultaneous production of renewable energy like H<sub>2</sub> from water or sacrificial agents (pollutants). Many researchers have developed the simultaneous degradation of pollutants and production of hydrogen considering its reliability (Cao et al., 2020; Jia et al., 2021; Zhu *et al.*, 2022). TiO<sub>2</sub> is the semiconductor most widely used as a photocatalyst due to its cost-effectiveness, nontoxicity, stability, and activity (Ratnawati et al., 2014).

Electrocoagulation and photocatalysis have been used to degrade dyes, by either performing photocatalysis first followed by electrocoagulation or vice versa managed to achieve 90% pollutant removal (Boroski et al., 2009; Santos et al., 2015; Ates et al., 2017; Dindas et al., 2020). Unfortunately, the combination of the two processes is rather rare and yet to be studied intensively. To our knowledge, there is no report in the literature on the simultaneous decolorization of wastewater and H<sub>2</sub> production from tartrazine conducted in one integrated reactor. In such a system, the dye is adsorbed by the coagulant formed in the electrocoagulation system and degraded by the photo generated OH• radicals. At the same time, H<sub>2</sub> is produced by the electroreduction of H<sup>+</sup> in the cathode and photocatalytic reduction on the surface of the photocatalyst. The simultaneous process between electrocoagulation and photocatalysis proposed in this study is expected to provide a more sustainable system as saturation of adsorbed pollutants can be avoided. Thus, the combined process has the potential of effective, sustainable, simultaneous decolorization of tartrazine production of hydrogen. In our previous study, we applied the same strategy for other pollutants with encouraging results (Sharfan et al., 2018). We also performed the combined process in a simple reactor using TNTA as the photocatalyst and coagulation at a low voltage of 5, 10, and 15 Volt (Slamet &

Kurniawan, 2018), and CuO-TNTA hybrid material at specific loading of 0.06 M at pH (11), and 20 V (Pelawi *et al.*, 2019).

In the present work, we investigate the combination of electrocoagulation and photocatalytic system in an integrated photoreactor for the degradation of tartrazine and generation of H<sub>2</sub> in different pH values and at different applied voltages. We also look at the effects of CuO loading in CuO-TiO<sub>2</sub> composites on the device performance. The samples were characterized using SEM, EDX, TEM, UV-Vis DRS, and XRD, the results of which are used to examine the effects of the important parameters on tartrazine removal and hydrogen production.

#### 2. LITERATURE REVIEW 2.1. Electrocoagulation

The electrocoagulation process, а combination of coagulation, flotation, and electrochemistry, is the coagulation of colloidal particles (pollutants) in water or wastewater in the application of electric current generated from direct current (DC) power (Syaichurrozi et al., 2021). This method is widely used to treat wastes originating from a wide range of industries such as food (Byoud et al., 2017), dyes (Anantha Singh, & Ramesh, 2013), and distillery spent wash (Syaichurrozi et al., 2021). The process consists of three steps, namely electrolysis, coagulation, and flotation (Hashim et al., 2020). During these processes, Al, or Fe dissolves in the anode to form Al<sup>3+</sup> and Fe<sup>2+</sup> allowing electric current to flow while water is reduced in the cathode to generate H<sub>2</sub> and OH<sup>-</sup> ions. Al or Fe reacts with  $OH^{-}$  ion to form in situ Al (OH)<sub>3</sub> or Fe (OH)<sub>2</sub> coagulants that can adsorb pollutants while H<sub>2</sub> is produced through water electrolysis. In this case, H<sub>2</sub> helps to float the flocculated pollutants on the surface of wastewater to generate scum (Syaichurrozi et al., 2021). The fact that this process also produces H<sub>2</sub> opens another opportunity in finding an alternative to the green production of clean fuel. With

industrial development, the need for  $H_2$  as renewable energy is very crucial to replace fossil fuels. Therefore, this approach can potentially synthesize an integrated system that simultaneously eliminates pollutants and generate  $H_2$ .

The reactions that occur in the electrocoagulation are as follows:

Anode:  $Al(s) \rightarrow Al^{3+}(aq) + 3e$ - (1)

Cathode:  $2H_2O$  (aq) +  $2e \rightarrow 2OH^-$  (aq) +  $H_2$ (g) (2)  $Al^{3+}$  (aq) +  $3OH^-$  (aq)  $\rightarrow Al(OH)_3$ (s) (3)

 $AI(OH)_3$  (s)+ pollutant  $\rightarrow$  (Pollutant-AI(OH)\_3) (s) (4)

# 2.2. Photocatalysis

Photocatalysis, combination of а photochemical and catalytic processes, is a chemical transformation process that utilizes photon energy from light to activate the semiconductor (Muttagin et al., 2022). The irradiation of semiconductor TiO<sub>2</sub> with photons (hv) at energy equal to or greater than its bandgap can excite the electrons in the valence band (VB) to the conduction band (CB), thereby, leaving positively charged holes (h<sup>+</sup>) in the VB. Three possibilities will occur in the electron and hole pairs, namely: (a) some pairs recombine TiO<sub>2</sub> particles in (volume/bulk recombination), (b) some pairs recombine on the TiO<sub>2</sub> surface (surface recombination), and (c) a small number of pairs can react with donor (D) and acceptor (A) species adsorbed on the particle surface. If the electrons and holes reach the surface of the photocatalyst, they later react with water and pollutants as follows:

 $TiO_2 + 2h\nu \rightarrow 2h^+ + 2e^- \tag{5}$ 

$$H_2O + h^+ \rightarrow OH \bullet + H^+ \tag{6}$$

$$OH \bullet + dye \text{ (pollutant)} \rightarrow CO_2 + H_2O$$
 (7)

$$2H^+ + 2e^- \to H_2(g) \tag{8}$$

 $TiO_2$  has many applications such as photocatalyst in pollutant degradation,  $H_2$ generation from various biomass, dyesensitized solar cells, and water splitting (Ratnawati et al., 2014). In pollutant degradation, several factors affect process efficiencies such as pollutant concentration, solar intensity, the amount of photocatalyst (Nandiyanto et al., 2016), and crystallite size (Nandiyanto et al., 2020). TiO<sub>2</sub> can also be used as raw material for carbon coated Ti<sub>4</sub>O<sub>7</sub> nanoparticles for electrocatalyst support (Kartikowati et al., 2021). However, the use of TiO<sub>2</sub> still holds some downsides in terms of electron-hole recombination, inactivity under visible light illumination due to a large band gap (3.2 eV), and limited surface area. These limitations could potentially disrupt the photocatalytic performance in its applications. Therefore, some modifications have which been sought, include morphological engineering to form TiO<sub>2</sub> nanotube arrays, non-metal (e.g. C, N, F, or B) (Ratnawati et al., 2014) and noble metal (e.g. Pt, Pd, Au, or Fe) doping (Slamet et al., 2017; Muttagin et al., 2022), deposition of transition metal oxide CuO on TiO<sub>2</sub> (Sang et al., 2019; Elysabeth et al., 2021), and sensitization with WO<sub>3</sub>, CdS, CdSe, or PbS to reduce recombination and improve the capability of harnessing visible light (Elangovan et al., 2021).

TiO<sub>2</sub> nanotube arrays (TNTA) are usually synthesized via an anodization process in an electrolyte containing fluoride ions. Such materials are preferred due to their ability to generate large surface area while the electrolyte solution for the anodization can also contain a precursor to the non-metal dopant which can reduce the bandgap energy of TiO<sub>2</sub> (Ratnawati et al., 2014). Moreover, CuO has also been deposited on TNTA via a successive ionic layer adsorption reaction (SILAR) method to reduce the electron-hole recombination and narrow the bandgap based on the fact that this technique exhibits better performance when compared to others as previously reported (Elysabeth et al., 2021). CuO is an inexpensive and environmentally friendly material that can trap the photogenerated electrons to efficiently suppress electron-hole recombination (Momeni, 2015: Zangeneh et al., 2020). Furthermore, its narrow band gap (1.7 eV) also indicates its ability to act as a sensitizer for visible light illumination (Sun et al., 2013; Momeni et al., 2015; Zangeneh et al., 2020). As mentioned previously, some researchers have performed waste combination treatment using а of photocatalysis electrocoagulation and sequentially or simultaneously in one integrated reactor which can be presented in Table 1. Although the treatment process is similar, the conditions and variations of the process are different.

## 3. METHOD

## 3.1. Materials

Tartrazine dye (C1<sub>6</sub>H<sub>9</sub>N<sub>4</sub>Na<sub>3</sub>O<sub>9</sub>S<sub>2</sub>), glycerol, sodium hydroxide (NaOH), ammonium fluoride (NH₄F), nitric acid (HNO<sub>3</sub>), hydrochloric acid (HCl), and copper (II) trihydrate (Merck, PA) nitrate were purchased from Merck and used without further purification. All solutions were prepared using high purity distilled water. Thin Ti foils with a thickness of 0.025 mm were used as a base on which TiO<sub>2</sub> nanotube arrays are grown, while aluminium plates with a thickness of 0.05 mm, and stainless steel 316 (SS-316) with a thickness of 1 mm were used as the anode and cathode, respectively.

#### 3.2. Synthesis of TNTA and CuO-TNTA

The Ti foil with the size of 8 cm x 2.5 cm was cleaned and washed with DI water before chemically polished using a mixture of HF, HNO<sub>3</sub>, and water with a volume ratio of 1:3:46 to remove any impurities. TNTA was obtained via an anodization method in a cell containing an electrolyte comprising 160-mL glycerol solution, 0.5 w% NH<sub>4</sub>F, and 25 v/v% DI water. The solution was continuously stirred for at least 10 mins. In this setup, a 2mm-thick Pt plate with a size of 3 cm × 1.5 cm was employed as a cathode. A constant 50-V potential difference was applied using a DC power supply (Escord 6030SD) for 2-h carried anodization out at room temperature.

The CuO-TNTA was obtained by depositing CuO on TiO<sub>2</sub> nanotube arrays through the successive ionic layer adsorption and reaction (SILAR) method. Firstly, the TNTA was immersed in a Cu (NO<sub>3</sub>)<sub>2</sub> solution with various concentrations of 0.04 M, 0.05 M, and 0.06 M at 75°C for 10 mins. The plate was then transferred to DI water for 30 s before being dried at room temperature for 30 s. These processes constitute one SILAR cycle. The deposition of CuO to TNTA was performed for 20 SILAR cycles. All samples were then annealed at 500°C for 3 h under atmospheric ambiance.

photocatalysis				
Pollutants type	Treatment processes	Researchers		
Olive washing	Photocatalysis followed by	Ates <i>et al.,</i> 2017		
wastewater	electrocoagulation or vice versa			
Pharmaceutical and	Photocatalysis followed by	Boroski <i>et al,</i> 2009		
cosmetic wastewater	electrocoagulation or vice versa			
Pharmaceutical	Combination of electrocoagulation,	Dindas <i>et al,</i> 2020		
wastewater	electro-fenton and photocatalytic			
Dye	Electrochemical process and	Santos et al., 2015		
	heterogeneous photocatalysis			
Batik industry waste	Combination of electrocoagulation	Safran <i>et al.,</i> 2018		
	and photocatalysis			
Tartrazine	Combination of photocatalysis-	Slamet and Kurniawan,		
	electrocoagulation	2018; Pelawi <i>et al.,</i> 2019		
Ciprofloxacin and	Combination of photocatalysis-	Muttaqin <i>et al.,</i> 2022		
methylene blue	electrocoagulation			

Table 1.         Waste treatment using a combination of ele	ectrocoagulation and
nhotocatalysis	

#### 3.3. Characterizations

The morphology of the synthesized TNTA and CuO-TNTA samples was examined by a scanning electron microscope (SEM, JSM-IT300 InTouchScope<sup>™</sup> 15 kV and 7 mA) equipped with energy dispersive X-ray (EDX) spectroscopy to characterize the elemental composition. Nanostructural features of the samples were also probed using transmission electron microscope (TEM, FEI Tecnai type G2-STWIN) operating at 200 kV along with further analysis of selected area electron diffraction (SAED). The crystallite properties of the samples were identified by an X-ray diffractometer (XRD) (PAN analytical Empyrean diffractometer) with a Cu anode tube ( $\lambda$  = 0.15406 nm) operating at 40 kV and 30 mA, scanned within the 2 $\theta$  range of 20 – 65°.

Accordingly, the crystallite size was estimated from the full-width half-maximum (FWHM) of the XRD peaks using the Scherrer equation. The optical properties and the bandgap values of the samples were estimated using the Kubelka-Munk functions from the obtained UV-visible diffuse reflection spectra (UV-Vis DRS, Harrick Scientific, Agilent Cary 600 UV-Vis, DRS) in the range of 300-700 nm. Dye absorption was measured using a UV-Vis spectrophotometer (Shimadzu UV 1600, Japan) and the produced H<sub>2</sub> from the reaction system was detected employing chromatography gas (GC) (Shimadzu GC-8A) with a 5A Molecular Sieve (MS) column and high purity argon used as the carrier gas.

#### 3.4. Electrocoagulation Test

Simultaneous decolorization of tartrazine and production of  $H_2$  was performed in an acrylic reactor equipped with a power supply, Tedlar bag, Quartz tube, and Pyrex tube. A 316 stainless steel plate (thickness × length × wide = 1 × 11 × 2.5 cm) used as the cathode was placed between two aluminum plates (thickness × length × wide =  $0.05 \times 11 \times 2.5$ cm) which are assigned as anodes. The Pyrex tube mounted on the SS-316 plate was connected to the Tedlar bag as a hydrogen collector. The reactor is filled with 400 mL of 20-mg/L tartrazine solution at different pH values, i.e. 11 (alkaline) and 4 (acidic). Samples were collected every hour to be analyzed using UV-Vis spectrophotometry at the wavelength of 405 nm for the solution of pH = 11 and 427 nm for the solution of pH = 4. At the cathode side, hydrogen produced was measured using gas chromatography (GC).

# 3.5. Photocatalyst Performance Test in the Electrocoagulation-Photocatalytic System

The effects of combining the electrocoagulation photocatalytic and processes were evaluated by adding TNTA or CuO-TNTA to the reactor system (depicted in Figure 1), irradiated by UV lamps (Sankyo Denki, 80 W, 365-nm wavelength). The aluminum plates and SS-316 for electrocoagulation tests and TNTA photocatalysts were placed in an acrylic reactor connected to a Tedlar bag which was used as a gas reservoir. The reactions were conducted in 4 hours and the effects of pH (i.e. 4 and 11) and the applied voltage (i.e. 20, 30, 40, and 50 V) were studied. Meanwhile, the depletion of tartrazine concentration was monitored using UV-Vis а spectrophotometer (Shimadzu UV 1600, Japan) and calculated using the following Eq. (9):

% decrease =  $\frac{C_{initial} - C_{final}}{C_{initial}} \times 100\%$  (9) where  $C_{initial}$  and  $C_{final}$  are the initial and final concentrations of tartrazine, respectively. 391 | Indonesian Journal of Science & Technology, Volume 7 Issue 3, December 2022 Hal. 385-404



Figure 1. Reactor vessel for the combination of electrocoagulation and photocatalytic process.

The kinetics of the degradation has been described by the Langmuir-Hinshelwood kinetic model (Nandiyanto *et al.,* 2020) (Eq. 10) as follows:

$$-\frac{dC}{dt} = \frac{k_T.K_c.C}{1+K_c.C} \tag{10}$$

where C is the concentration of tartrazine at a specific time t,  $k_T$  is the apparent reaction rate constant,  $K_C$  is the apparent equilibrium adsorption coefficient. When the initial reactant concentration (C<sub>0</sub>) is low, the expression model of Eq. 10 becomes:

$$-\frac{dC}{dt} = kC^n \tag{11}$$

For first-order degradation kinetics, it can be calculated by integrating the above Eq. (11) with order n = 1, therefore Eq. (11) becomes:

$$\ln\left(\frac{c_t}{c_0}\right) = -k_1 t \tag{12}$$

where  $C_t$  is the concentration at time t,  $C_o$  is the initial concentration, and  $k_1$  is a kinetic constant for order 1. Plotting of Eq. (12) namely  $\left(\ln\left(\frac{C_0}{C_t}\right)$  vs t will obtain  $k_1$  as a slope.

## 4. RESULTS AND DISCUSSION 4.1. Photocatalyst Characterization

Micrographs depicting the surface morphology of TNTA and CuO-TNTA composites are shown in **Figure 2**.

Superficially, no significant differences were observed in the morphological structure of all four samples. However, upon further scrutiny, it was found that CuO deposition induces a slight increase in the inner diameter of the tubes as Cu concentration increases.

The wall thickness of the tubes, on the other hand, remains relatively unaffected, as presented in Table 2. It is well documented that water content and mechanical stirring during anodization may contribute to the eventual dimension of nanotubes (Elysabeth et al., 2021), while the nanotubular structure of TiO<sub>2</sub> is dependent on the competition between the formation of oxides on the uppermost layer of the plate and the dissolution into the electrolyte solution (Ratnawati et al., 2014). Upon increasing the concentration of CuO precursor (Cu(NO<sub>3</sub>)<sub>2</sub>) from 0.04 to 0.06 M, the inner diameter of the tubes increases, possibly due to the sintering effects of calcination on particle size. The concentration of precursor solution of Cu(NO<sub>3</sub>)<sub>2</sub> might affect the mobility of CuO incorporating amorphous regions. Upon calcination, the amorphous phase is converted to a crystal phase, thereby increasing the conductivity of CuO which further causes an increase in the tube diameter.



**Figure 2.** SEM image of (a) Amorphous TNTA, (b) 0.04 M of CuO-TNTA, (c) 0.05 M of CuO-TNTA, and (d) 0.06 M of CuO-TNTA.

**Table 2.** The average tube diameter, average tube wall thickness, and EDX analysis ofvarious photocatalyst.

	Average tube Average tube		% Weight of Component				
Photocatalyst	inner diameter (nm)	wall thickness (nm)	Cu	Ті	0	С	F
TNTA (amorphous)	134	47	0	53.15	28.74	17.2	0.96
0.04 M of CuO-TNTA	149	44	0.40	60.67	30.23	7.58	1.13
0.05 M of CuO-TNTA	158	50	1.09	61.25	30.06	6.47	1.40
0.06 M of CuO-TNTA	166	52	1.68	58.52	33.12	5.97	0.68

It is important to note that the amorphous TNTA comprises porous structures which become denser after annealing. The results of our previous studies also found that the tube diameter of crystallite TNTA became larger after amorphous TNTA was calcined at 500°C (Ratnawati *et al.*, 2015). CuO bonding on the TNTA surface might also change the molecular configuration, which is indicated by the increase in the inner diameter of the tube. Meanwhile, the TiO<sub>2</sub> nanotube arrays surface in the amorphous form was covered by the remaining glycerol electrolyte solution as indicated by rather high carbon content, resulting from the decomposition of glycerol into carbon as indicated by the EDX analysis results, shown in **Table 2**. EDX analysis also identifies flour content in the nanotubes, which is likely to be originated from NH<sub>4</sub>F leftover (Ratnawati *et al.*, 2014). Importantly, the content of Cu in CuO-TNTA composites is found to be 0.4%wt, 1.09%wt, and 1.68%wt, corresponding to  $Cu(NO_3)_2$  concentrations of 0.04, 0.05, and 0.06 M, respectively.

The procedures for interpreting and calculating the average tube inner diameter of TNTA (Figure 2) using SEM are (1) determination of the morphological shape (irregular tube) and (2) analysis of scale bar/diameter size. The second step includes identifying the scale bar on the SEM image and comparing it with the diameter size of TNTA, measuring the minimum/maximum Feret diameter according to the number of samples, calculating the average Feret diameter of each sample [(d max + d min)/2], and finally calculating the average of Feret diameter for all samples as shown in Table 2 (Yolanda and Nandiyanto, 2022). Tube wall thickness was also calculated by measuring the thickness of each tube and then averaged according to the number of existing tubes.

The nanostructure of the composites was further probed utilizing TEM and SAED analyses, presented in Figure 3. From the micrograph depicted in Figure 3a, it is inferred that Cu was successfully deposited on TiO<sub>2</sub>, corroborating the finding from EDX CuO analysis. The nanoparticles are distributed on the wall of the nanotubes with a thickness of 22-26.24 nm and an inner diameter of 244.9-248.9 nm. However, the average values of wall thickness and inner diameter are lower, as informed in Table 1. This may indicate that the closer the tubes are to their bottom part, the larger their diameter would be. The longer the anodizing time, the more [TiF6]<sup>-2</sup> dissolves from the inner part of the tubes, thereby increasing the inner tube diameter. This condition imposes a challenge for CuO to enter the inner side of the tubes. Figure 3a shows that CuO is well distributed on the outer surface of TNTA. Figure 3b reveals the interplanar distance d(111) at 0.22 nm that originates from the CuO crystal region, conforming to the XRD signal of CuO at 20 of ca. 38.77°. Figures 3b and 3d depict the crystal lattice of TiO<sub>2</sub> with a d-spacing of 0.35 nm, attributable to (101) anatase crystallite phase. To further

investigate the crystal structure of the synthesized nanocomposites, SAED analysis was sought and the patterns are shown in **Figure 3c**, illustrating the calculated interplanar distances (dhkl) in the cases of CuO (111) and TNTA (101), (004), (200) and (105).

The XRD patterns of TNTA and CuO-TNTA samples are illustrated in Figure 4 to scrutinize their crystallite properties studied using XRD as depicted in Figure 4. The diffraction signals emerging at  $2\theta$  of 25.52, 37.98, 48.24, and 54.08° correspond to the anatase crystallite according to the Miller indices of (101), (004), (200), and (105), respectively (JCPDS No. 21-1272) (Meng et al., 2016; Elysabeth et al., 2021), while other peaks are attributable to the metallic titanium. On the other hand, no signal of rutile phase is observed, e.g. at 27.37, 36.02, 41.16, or 56.53° with diffraction fields of (110), (101), (111), and (220) (JCPDS No. 21-1276). Interestingly, the increased amount of Cu in the composite led to the higher peak intensity of the anatase phase, indicating that the crystal formation is somewhat more effective in the case of Cu-deposited nanotubes. This may be associated with the high thermal conductivity of CuO which allows more effective heat conduction during the calcination of the samples (Ahn et al., 2013; Elysabeth et al., 2021). The crystallite size of the TNTA samples was estimated using the Debye–Scherrer equation (Elysabeth et al., 2021), revealing values in the range of 26.9 – 28.5 nm, as inferred from Table 3. A weak diffraction peak is detected at 20 of ca. 38.77° assigned to the (111) plane of CuO crystal according to JCPDS 8012 68 (Raul et al., 2014). This phenomenon agrees with EDX results, in which the low amount of Cu element was confirmed. Moreover, the low Cu concentrations also provide an advantage since they did not lead to a shading effect thereby, not reducing the active site of the TiO<sub>2</sub> nanotube arrays photocatalyst (Janczarek & Kowalska, 2017).



Figure 3. TEM image a) CuO distribution, b) and d) lattice structure, c) SAED patterns of TNTA-CuO Hybrid Structure.



**Figure 4.** XRD patterns of various photocatalysts samples (a) TiO<sub>2</sub> nanotube arrays (TNTA), (b) 0.04 M of CuO-TNTA, (c) 0.05 M of CuO-TNTA, and (d) 0.06 M of CuO-TNTA.

As an illustration, the crystallite size of TNTA can be calculated using Debye Scherrer's Eq. (13) as follows (Fatimah *et al.*, 2022):

$$D = \frac{K\lambda}{\beta \cos\theta} \tag{13}$$

with D = crystal size (nm), K = Scherrer constant = 0.9,  $\lambda$  = wavelength of X-ray radiation used = 0.15406 nm,  $\beta$  = Full Width at half maximum (FWHM) = 0.286 (should be

converted to radian), and  $\theta$  = the peak position of the TNTA in XRD pattern = (25.52/2) (should be converted to radian). From this formula, the crystallite size for TNTA is 28.5 nm as shown in **Table 3**.

**Figure 5** represents the UV-Vis absorption spectra of different photocatalyst samples. The bandgap is evaluated by the Kubelka–Munk equation (Elysabeth *et al.*, 2021) and is presented in **Table 4**.

The results indicate that all samples exhibit enhancement in terms of photoresponse, as the onsets shift to the visible light region (> 400 nm) while the addition of CuO imposes bandgap values of 3.03, 2.98, and 2.96 eV, lower than the 3.16 eV recorded for the pure TiO<sub>2</sub> nanotube. The redshift can be reasoned by the presence of the CuO in TiO<sub>2</sub> nanotubes, possessing a bandgap of 1.2 eV (Sun *et al.*, 2013). The red shift is more apparent in the case of CuO-TNTA with higher content of CuO while the lower content of CuO does not affect the optical properties significantly.

The UV-Vis Diffuse Reflectance Spectroscopy (DRS) method is based on measuring the UV-Vis intensity reflected by the sample. When the light (ultraviolet and/or visible) is irradiated by the material, some of it is absorbed, reflected, and transmitted in the form of spectra. The absorption of light causes the excitation of electrons from the ground to an excited state (Pratiwi and Nandiyanto, 2022). Using the Kubelka-Munk function F(R) and Tauc plot, the band gap energy (Eg) of the photocatalyst can be determined by Eq. (14) as follows:

$$[F(R)hv]^{1/2} = K(hv - Eg)$$
(14)

with  $F(R) = (1-R)^2/2R$ , R = reflectance, hv = photon energy, and K = constant characteristic of TiO<sub>2</sub>. For TNTA, a plot of  $[F(R) hv]^{1/2}$  vs. hv must show a linear region just above the optical absorption edge (Ratnawati, 2014). The band gap energy can be found with the extrapolation of the linear portion of a Tauc plot to the hv axis, and the result is depicted in **Table 4**.

Table 3. The crystal size of various nanocomposites.

Nanocomposites	Anatase crystal size (nm)
TNTA (crystal)	28.5
0.04 M of CuO-TNTA	27.8
0.05 M of CuO-TNTA	27.0
0.06 M of CuO-TNTA	26.9



**Figure 5.** The UV-Vis DRS absorbance of different photocatalyst samples (a) TiO<sub>2</sub> nanotube arrays (TNTA), (b) 0.04 M of CuO-TNTA, (c) 0.05 M of CuO-TNTA, and (d) 0.06 M of CuO-TNTA.

Types of Nanocomposites	Band-Gap Energy (eV)	Wavelength (nm)
TNTA	3.16	392
0.04 M of CuO-TNTA	3.03	409
0.05 M of CuO-TNTA	2.98	416
0.06 M of CuO-TNTA	2.96	419

 Table 4. Band-gap energy of various nanocomposites.

## 4.2. Photocatalytic Test on Tartrazine Decolorization

Figure 6A depicts the photodegradation of tartrazine for two different pH values, in which it is evident that the photo-induced decolorization favors high pH. The adsorption-desorption properties on the surface of the catalysts are significantly affected by pH. This was related to the fact that the TiO<sub>2</sub> photocatalyst was negatively charged in the alkaline conditions due to the reaction between hydroxyl ions (OH<sup>-</sup>) and h<sup>+</sup> to form hydroxyl radicals (OH•), which subsequently attack tartrazine, as also reported by previous researchers (Gupta et al., 2011).

Under acidic conditions, the number of hydroxyl ions is small, so the formation of hydroxyl radicals is limited. As a result, under acidic conditions, the reaction rate of the photocatalytic process is relatively slow. The photodegradation of tartrazine at pH = 11 for different photocatalyst samples is presented in **Figure 6B**.

The photo-induced decolorization of tartrazine is positively correlated with the amount of CuO present in CuO-TNTA composites. The highest rate of decolorization was obtained by the use of CuO-TNTA prepared with 0.06 M of Cu precursor, offering 64% degradation of

tartrazine over 12 h illumination. In this case, CuO plays an important role in terms of inhibiting charge recombination, thereby facilitating faster separation and transfer of electrons and holes (Anantha Singh, & Ramesh, 2013).

Considering the band alignment between TiO<sub>2</sub> and CuO, we believe that the photoexcited electrons generated in the conduction band of TiO<sub>2</sub> are thermodynamically feasible to move to the more positive conduction band of CuO. Conversely, the holes generated in the valence band of CuO are transferred to the more negative valence band of TiO<sub>2</sub>. The relatively low rate of photocatalytic reaction is most likely due to the limited surface area of the photocatalyst films (ca. 20 cm<sup>2</sup>).

To calculate the photodegradation rate of tartrazine at various dopant CuO concentrations (**Figure 6B**), Eq. (12) was applied, and the results are depicted in **Table 5**.

The high value of the correlation coefficient ( $R^2$ ) indicates that statistically, the first-order kinetic model is following the experimental data. The greater the value of  $k_1$ , the faster the photodegradation rate which results in high removal efficiency. This condition was achieved by a photocatalytic process using 0.06 M of CuO-TNTA.



**Figure 6.** Photodegradation of tartrazine with 0.06 M CuO-TNTA at different pH (A) with pH = 4 (1), pH = 11 (2), and several photocatalysts (B) with TNTA (1), 0.04 M CuO-TNTA (2), 0.06 M CuO-TNTA (3) at pH = 11.

Table 5. Comparison of kinetic constants, k for the first-order reaction of tartrazine removal
at various photocatalyst.

Dhataataluata	first-order pseudo model			
Photocatalysis	k₁ (hours <sup>-1</sup> )	R <sup>2</sup>		
TNTA	0.0172	0.929		
0.04M CuO-TNTA	0.0272	0.924		
0.06M CuO-TNTA	0.0849	0.955		

## 4.3. Electrocoagulation Test of the Tartrazine Decolorization and H<sub>2</sub> Production

The decolorization of tartrazine through electrocoagulation was conducted in a reactor with an Al plate as the anode and SS 316 plate as the cathode. **Figure 7A** shows the decolorization of tartrazine at different voltages of electrocoagulation, offering tartrazine removal of 56, 71, 82, and 88% at 20, 30, 40, and 50 V, respectively.

The positive correlation between the voltage and the removal rate of the redox target is unsurprising, as the reaction rate is directly proportional to the current, and the current is positively correlated to the electrical driving force, which was also reported by other authors (Syaichurrozi *et al.*, 2021).

At higher voltage, more electrons are extracted from the anode to produce  $AI^{3+}$  from Al, which, subsequently forms  $AI(OH)_3$  serving as a coagulant. Furthermore, more

electrons are transferred to the inert cathode to produce  $H_2$  from the reduction of  $H_2O$  or protons.

**Figure 7B** displays the production of H<sub>2</sub> throughout 4 h operation, running at different voltages. It was found that the amount of H<sub>2</sub> generated from the processes is 1.52, 3.58, 10.86, and 17.03 mmol H<sub>2</sub> at 20, 30, 40, and 50 V, respectively. These results confirm the feasibility of the simultaneous removal of dye and production of fuel through the scheme proposed in this study. This result is following the findings that have been reported by previous researchers (Boroski *et al.*, 2009; Ates *et al.*, 2017; Syaichurrozi *et al.*, 2021).

To evaluate the tartrazine removal efficiency by electrocoagulation process at various voltages, the removal rates were calculated according to Eq. (12), and the results are in **Table 6**. From **Table 6**, it can be concluded that the higher the voltage, the greater the value of  $k_1$ , and therefore the rate of tartrazine removal is also faster.





**Figure 7.** Degradation of tartrazine (A)  $H_2$  production by electrocoagulation (B) as a function of time and at various voltages of 20 V (1), 30 V (2), 40 V (3), and 50 V (4) at pH = 11.

**Figure 8A** and **8B** respectively show the simultaneous decolorization of tartrazine and generation of  $H_2$  in different modes of operation, namely photocatalysis, electrocoagulation, and the combination of both. In terms of tartrazine removal, 60% removal was obtained in the case of electrocoagulation only and 31% in the case of photocatalysis only. Upon combining both processes, 80% removal of tartrazine is achieved throughout 4 h. Similarly, in terms of  $H_2$  production, the combination of

electrocoagulation and photocatalysis staggeringly generates 1.84 mmol of  $H_2$ , much superior to those obtained by the operation of electrocoagulation (0.99 mmol) and photocatalysis (0.08 mmol). Since the electrocoagulation-photocatalysis

Combination managed to nearly double the total production of  $H_2$  of the individual processes, the synergetic effect of both processes is plausible. It is likely that, in the case of the combined process, OH<sup>-</sup> reacts not only with Al<sup>3+</sup> but also with photo-excited holes to generate hydroxyl radicals. Combined with the electron-trapping role performed by CuO in CuO-TNTA composite, this scheme allows suppression of electronhole recombination (Zangeneh *et al.*, 2020).

**Figure 9** represents the same comparative study of different operation modes for the decolorization of tartrazine, operating at a higher voltage (50 V), which further corroborates the effectiveness of the combined process, and the removal rates are

presented in **Table 7**. The combination of photocatalysis and electrocoagulation processes has the highest rate constant for decreasing tartrazine concentration (**Table 7**). This means that this process combination provides the highest efficiency compared to other processes. This finding agreed with the results previously reported (Muttaqin *et al.*, 2022) when they used different types of waste.

Table 6. The adsorption rate constant of tartrazine at various voltages.

Electrocoagulation		first-order pseudo model		
	Voltage	k₁ (hours⁻¹)	R <sup>2</sup>	
	20 V	0.3275	0.908	
	30 V	0.3096	0.991	
	40 V	0.5041	0.970	
	50 V	0.5595	0.942	







**Figure 9.** Degradation of tartrazine at pH = 11, 50 V as a function of time at (1) photocatalytic process with CuO 0.06 M-TNTA, (2) electrocoagulation, and (3) combination of electrocoagulation–photocatalytic.

Treatment Process	first-order pseudo model	
	k₁ (hours⁻¹)	R <sup>2</sup>
Photocatalytic (P)	0.0272	0.924
Electrocoagulation (E)	0.5595	0.942
Combination of P and E	1.2022	0.998

**Table 7.** The comparative value of the rate constant at different operation modes forthe decolorization of tartrazine.

Figure 10 shows the scheme of the combined processes of electrocoagulation and photocatalysis. In this scheme, tartrazine is degraded by the adsorption of Al(OH)<sub>3</sub> in the electrocoagulation process and it oxidizes by  $\bullet OH$  or  $\bullet O^{2-}$  radicals in the photocatalytic process simultaneously. At the same time, H<sub>2</sub> produces by the reduction of H<sup>+</sup> in the cathode and on the photocatalyst surface. The glass sheath protects the cathode of SS 316 and CuO-TNTA photocatalyst plates to provide H<sub>2</sub> is collected and thereby the measurement becomes more accurate. In this combination process integrated into one reactor, operating conditions affect the efficiency of the waste treatment and H<sub>2</sub> production namely pH (Ates et al., 2017), Voltage (Boroski et al., 2009; Ates et al., 2017; Syaichurrozi *et al.*, 2021), electrode materials, distance of the electrodes (Amri et al., 2020), amount of the photocatalyst, the crystallite size, the concentration of waste (Nandiyanto et al., 2016, Muttaqin et al., 2022), and type of wastes (Safran et al., 2018; Dindas et al., 2020).

#### **5. CONCLUSION**

This study reports the combination of electrocoagulation and photocatalysis to simultaneously eliminate tartrazine dye and produce hydrogen in an integrated reactor. The deposition of CuO on TNTA photocatalyst using the SILAR method was successfully conducted, as confirmed by EDX analysis, TEM imaging, and SAED analysis. Upon the addition of CuO on TNTA, the redshift of the optical onset and bandgap lowering was also CuO-TNTA observed. The composite improves the photocatalytic activity of TiO<sub>2</sub>. The combination of electrocoagulation and photocatalysis in eliminating tartrazine as well as producing  $H_2$  is superior to each process, resulting in 80% tartrazine removal and 1.84 mmol H<sub>2</sub> productions. The significant improvement observed in this study suggests a synergetic effect between both processes. The results reported in this study are expected to pave the way to an integrated system capable of effectively removing pollutants, while, at the same time, producing  $H_2$  as a green fuel.



**Figure 10**. The mechanisms used in the combination of electrocoagulation and photocatalytic process.

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#### 7. AUTHORS' NOTE

The authors declare that there is no conflict of interest regarding the publication of this article. The authors confirmed that the paper was free of plagiarism.

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